

# Chapter 4

## Sliding Mode Observers

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### 4.1 Introduction

Sliding mode techniques have been widely studied and developed for the control problem and observation in the occidental countries<sup>1</sup> since the works of Utkin [43]. As discussed by many authors [22, 40, 21, 37, 49, 50, 20, 4, 31, 24, 33], this methodology has several drawbacks in control design, adaptive control and observation. More particularly, several authors have used sliding observer for linear and nonlinear systems, and in many applications such as robotics [41, 12, 13, 28], mobile robots [5], AC motors [16, 17, 18] and converters [36].

This kind of observer is very useful and was developed for many reasons:

- to work with reduced observation error dynamics
- for the possibility of obtaining a step-by-step design
- for a finite time convergence for all the observables states
- to design, under some conditions, an observer for nonsmooth systems, and
- robustness under parameter variations is possible, if the condition (dual of the well-known matching condition) is verified.

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<sup>1</sup>It is important to highlight the paternity and the major contribution of the Russian school in the sliding mode domain.

Here, we highlight a few advantages of the sliding observer. One advantage is the possibility to design an observer for a system with an undetermined but bounded specific variable structure, however, throughout this chapter we choose to focus our attention on widening the class of considered systems in the design of the observer.

Historically, in nonlinear control theories, the problem of a nonlinear observer design with linearization of the observation error dynamics for a class of nonlinear systems, called *the input injection form*, has been investigated ([29, 45, 46]...). Some necessary and sufficient conditions to obtain such a form are given in [46]. From this form, it is “easy” to design an observer. Unfortunately, the geometric conditions to obtain this form are very often too restrictive with respect to the system considered. Thus, in [11] we have given an extension of the results obtained in [29, 30, 35, 45, 46], for systems that can be written in an output injection form to systems which can be written in the form of the output and the output’s derivative injection. We first recall this result and then we deal with a more general case, which is the *triangular observer form* [1]. Here, aiming for simplicity, we only present the case of single output system. The multi-output case may be found in [6], where the implicit triangular observer form is introduced in order to take into account the fact that the information quantity given by one output and its derivatives may change along the state space. Roughly speaking, in the nonlinear case, in the neighborhood of  $x_0$ , information about the state can be given by the output  $y_1$  (one component of the output) and its derivative, and in another neighborhood of  $x_1$ , information can be given by  $y_2$  (another component of the output) and its derivative. In both forms considered in this presentation, input derivatives are prohibited. Indeed, if they are allowed it is possible to use the observer form proposed in [25] and in that case a sliding observer is also widely used (see for example [34]).

As in other chapters, some recall on high order sliding mode are given [31], then for the sake of clarity we do not present the high order sliding observer [7, 3, 7]. Moreover, we deferred some technical proofs to the appendix.

We find that it is important to end this introduction with the following warning: in this chapter we omit many interesting aspects, for example, the observer design without coordinate change [14], high gain [10], and noise sensibility [47]. The subject is too large and open, to be able to squeeze it in an introductory presentation. The main purpose of this chapter is to highlight the utilities and difficulties of sliding mode technique for the observer design.

## 4.2 Preliminary example

In this section, the sliding observer is introduced based on a simple academic example. Let  $\Sigma$  be the system:

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= f(x_1, x_2) \\ y &= x_1\end{aligned}\tag{4.1}$$

where  $x \in \mathbb{R}^2$  and  $y \in \mathbb{R}$  is the output and the function  $f(x_1, x_2)$  is bounded ( $|f(x_1, x_2)| < B$ ) but not necessary smooth, thus (4.1) is a particular case of variable structure dynamics.

One wants to observe the state  $x$  with the additional constraint to obtain the real value of  $x_2$  in finite time. To do this, one uses a classical sliding mode observer, but completed with a new component  $\tilde{x}_2$ .

$$\begin{aligned}\dot{\hat{x}}_1 &= \hat{x}_2 + \lambda_1 \operatorname{sgn}(x_1 - \hat{x}_1) \\ \dot{\hat{x}}_2 &= f(x_1, \tilde{x}_2) + E_1 \lambda_2 \operatorname{sgn}(\tilde{x}_2 - \hat{x}_2) \\ \hat{y} &= \hat{x}_1 \\ \dot{\tilde{x}}_2 &= \hat{x}_2 + E_1 \lambda_1 \operatorname{sgn}(x_1 - \hat{x}_1)\end{aligned}\tag{4.2}$$

where  $\hat{x}$  represents the estimated value of  $x$  and  $E_1 = 1$  if  $x_1 = \hat{x}_1$  else  $E_1 = 0$  and sign denote the usual sign function.

From (4.1) and (4.2), the error observation ( $e = x - \hat{x}$ ) dynamics are:

$$\begin{aligned}\dot{e}_1 &= e_2 - \lambda_1 \operatorname{sgn}(e_1) \\ \dot{e}_2 &= f(x_1, x_2) - f(x_1, \tilde{x}_2) - E_1 \lambda_2 \operatorname{sgn}(\tilde{x}_2 - \hat{x}_2)\end{aligned}\tag{4.3}$$

Considering the nonempty manifold  $S = \{e/e_1 = 0\}$  and the Lyapunov function  $V = \frac{1}{2}e_1^2$ , one proves the attractivity of  $S$  as follows. One gets:  $\dot{V} = e_1 e_2 - \lambda_1 e_1 \operatorname{sgn}(e_1)$ , which verifies the inequality  $\dot{V} < 0$  when  $\lambda_1$  is chosen such that  $\lambda_1 > |e_2|_{max}$  (where  $|e|_{max}$  denotes the maximal value of  $e$ ,  $\forall t \in [0, \infty]$ ). As one uses a  $\operatorname{sgn}$  function and as the Lyapunov function  $V$  is decreasing, one obtains the convergence to the sliding surface  $S = 0$  in finite time  $t_0$  (and moreover, we have  $|e|_{max} = |e|_{max}^{t_0}$  and  $|e|_{max}^{t_0}$  is the maximal value of  $e$ ,  $\forall t \in [0, t_0]$ ). Thus, for  $\lambda_1 > |e_2|_{max}$ ,  $\hat{x}_1$  converges to  $x_1$  in finite time and remains equal to  $x_1$  for  $t > t_0$ .

Moreover, one also has that  $\dot{e}_1 = 0 \forall t > t_0$ , so that from (4.3),

$$e_2 = \lambda_1 \operatorname{sgn}(e_1)\tag{4.4}$$

Therefore, the observer output,  $\tilde{x}_2 = \hat{x}_2 + \lambda_1 \operatorname{sgn}(e_1)$  is equal to  $x_2 \forall t > t_0$ .

**Remark 31** *This is obviously only true without any noise measurement, but this difficulty may be partially overcome by a sgn function modification (see [47] for analysis and design of observer with respect to noise) or by high order sliding mode [31].*

Up to now, we proved for the system (4.1) that the observer (4.2) is suitable to give all the values of the state in finite time.

The condition  $\lambda_1 > |e_2|_{max}$  can only be verified if  $e_2$  has stable dynamics, which is fulfilled after  $t_0$  for  $\lambda_2 > 0$ , where we have

$$\dot{e}_2 = f(x_1, x_2) - f(x_1, \tilde{x}_2) - E_1 \lambda_2 \operatorname{sgn}(\tilde{x}_2 - \hat{x}_2)$$

with  $\tilde{x}_2 = x_2$  and  $E_1 = 1$  then

$$\dot{e}_2 = -\lambda_2 \operatorname{sgn}(e_2)$$

Therefore, one gets  $|e_2|_{max}^{t_0}$ , which is bounded by the way that  $t_0$  and  $f(x_1, x_2)$  are bounded. The observer (4.2) with assumptions  $\lambda_1 > |e_2|_{max}^{t_0}$  and  $\lambda_2 > 0$  ensures a finite time convergence of  $(e_1, e_2)$  to  $(0, 0)$ .

**Remark 32** *The time  $t_0$  can be very short because it is natural to initialize  $\hat{x}_1 = x_1$ .*

### 4.3 Output and output derivative injection form

Following, we recall some classical results on nonlinear observer theory.

#### 4.3.1 Nonlinear observer

First of all, we recall the definition of *observability indices*.

**Definition 33** [29] *Let the system*

$$\begin{aligned} \dot{x} &= f(x) \\ y &= h(x) \end{aligned} \tag{4.5}$$

*which is observable at  $x_0$  if there exists a neighborhood  $\mathcal{U}$  of  $x_0$  and  $p$ -tuple of integers  $(\mu_1, \dots, \mu_p)$  such that*

$$1) \mu_1 \geq \mu_2 \geq \dots \geq \mu_p \geq 0 \text{ and } \sum_{i=1}^p \mu_i = n.$$

- 2) After suitable reordering of the  $h_i$  at each  $x \in \mathcal{U}$ , the  $n$  row vectors  $\{L_f^{j-1}(dh_i) : i = 1, \dots, p; j = 1, \dots, \mu_i\}$  are linearly independent.
- 3) If  $l_1, \dots, l_p$  satisfies (i) and after suitable reordering the  $n$  row vectors  $\{L_f^{j-1}(dh_i) : i = 1, \dots, p; j = 1, \dots, l_i\}$  are linearly independent at some  $x \in \mathcal{U}$

then  $(l_1, \dots, l_p) \geq (\mu_1, \dots, \mu_p)$  in the lexicographic ordering  $[(l_1 > \mu_1)$  or  $(l_1 = \mu_1$  and  $l_2 > \mu_2)$  or... or  $(l_1 = \mu_1, \dots, l_p = \mu_p)]$ . The integers  $(\mu_1, \dots, \mu_p)$  are called the observability indices at  $x_0$ .

**Remark 34** In the nonlinear case, the previous notion of observability index is local. In the linear case, this notion is global.

As it is shown in [29, 30, 45], an interesting nonlinear systems is the output injection form without forced terms:

$$\begin{aligned} \dot{x} &= Ax + \phi(y) \\ y &= Cx \end{aligned} \quad (4.6)$$

where:

$$A = \left( \begin{array}{c|c|c} A_1 & 0 & 0 \\ \hline 0 & \ddots & 0 \\ \hline 0 & 0 & A_p \end{array} \right)$$

$$A_i \text{ is a } \mathbb{R}^{\mu_i \times \mu_i} \text{ matrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & \ddots & 1 \\ 0 & 0 & 0 \end{pmatrix} \quad (4.7)$$

$$\text{and } \left( \begin{array}{c|c|c} C_1 & 0 & 0 \\ \hline 0 & \ddots & 0 \\ \hline 0 & 0 & C_p \end{array} \right)$$

$C_i$  is a line vector  $\in \mathbb{R}^{\mu_i}$ , such that :  $C_i = (1, 0, \dots, 0)$ .

This is interesting because for such a class, one can design an observer that allows us to obtain an observation error with stable linear dynamics.

In fact, for the nonlinear observable system:

$$\begin{aligned} \dot{\xi} &= f(\xi) \\ y &= h(\xi) \end{aligned} \quad (4.8)$$

where  $f$  and  $h$  are smooth functions, necessary and sufficient conditions for the existence of a diffeomorphism  $x = \Phi(\xi)$  to transform the system (4.8) into (4.6) are given in [46].

**Theorem 35** [46] *There exists a change of coordinates transforming (4.8) into (4.6) only if there exists a  $p$ -tuple of integers  $(\mu_1, \dots, \mu_p)$ ,  $\mu_1 \geq \mu_2 \geq \dots \geq \mu_p$  such that we have the following:*

1) *If one denotes (with a possible reordering of the  $h_i$ )*

$$Q = \left\{ L_f^{j-1}(dh_i) : i = 1, \dots, p; j = 1, \dots, \mu_i \right\}$$

*then  $\dim \text{span } Q = n$  in a neighborhood of  $\xi^0$ .*

2) *If one denotes for  $j = 1, \dots, p$ ,*

$$Q_j = \left\{ L_f^{k-1}(dh_i) : \begin{array}{l} i = 1, \dots, p; \\ k = 1, \dots, \mu_j \end{array} \right\} - \left\{ L_f^{\mu_j-1}(dh_j) \right\}$$

*then  $\text{span } Q_j = \text{span } Q \cap Q_j$  for  $j = 1, \dots, p$ .*

**Theorem 36** [46] *There exists a change of coordinates transforming (4.8) to (4.6) if and only if 1. and 2. in the previous Theorem hold and, moreover, if there exists vector fields  $g^1, \dots, g^p$  satisfying:*

$$L_{g^i} L_f^{l-1}(h_j) = \delta_{i,j} \delta_{l,\mu_i}, \quad i, j = 1, \dots, p, \quad l = 1, \dots, \mu_i$$

*such that:  $[\text{ad}_{(-f)}^k g^i, \text{ad}_{(-f)}^l g^j] = \mathbf{0}$  for  $i, j = 1, \dots, p; k = 0, \dots, \mu_i - 1; l = 0, \dots, \mu_j - 1$ .*

Thus, it immediately follows:

**Corollary 37** *The conditions of Theorem 36 are sufficient to construct an observer that is asymptotically locally stable.*

### 4.3.2 Sliding observer for output and output derivative nonlinear injection form

In this section, one first constructs an asymptotically stable observer for the following class of systems called *output and output derivative nonlinear injection form*:

$$\begin{aligned} \dot{x}_i &= A_i x + \phi_i(y, \dot{y}) \\ y_i &= x_{i,1} \\ \dot{y}_i &= x_{i,2} \end{aligned} \quad \text{for } i = 1, \dots, p \quad (4.9)$$

with

$$\phi_i(y, \dot{y}) = \begin{pmatrix} \phi_{i,1}(y) \\ \phi_{i,2}(y, \dot{y}) \\ \vdots \\ \phi_{i,\mu_i}(y, \dot{y}) \end{pmatrix}$$

and all  $A_i$  matrix are of appropriated dimensions. Secondly, one exhibits the necessary and sufficient conditions under which the system (4.8) may be rewritten as (4.9). For the sake of simplicity, one introduces the following notations:

$$\begin{aligned} x_i &= (x_{i,1}, x_{i,2}, \dots, x_{i,\mu_i})^T \\ \tilde{x} &= (\tilde{x}_1, \tilde{x}_2, \dots, \tilde{x}_p)^T \\ \hat{x}_i &= (\hat{x}_{i,1}, \hat{x}_{i,2}, \dots, \hat{x}_{i,\mu_i})^T \quad \text{for } i = 1, \dots, p \end{aligned}$$

where  $\tilde{x}_i = \hat{x}_{i,2} + E_1 \lambda_{i,1} \text{sgn}(y_i - \hat{x}_{i,1})$  and  $E_1 = 1$  if  $(x_{1,1} - \hat{x}_{1,1}) = \dots = (x_{1,p} - \hat{x}_{1,p}) = 0$ , else  $E_1 = 0$ .

Let us construct for the system (4.9) the sliding observer:

$$\begin{aligned} \dot{\hat{x}}_{i,1} &= \hat{x}_{i,2} + \phi_1(y) + \lambda_{i,1} \text{sgn}(y_i - \hat{y}_i) \\ \dot{\hat{x}}_{i,2} &= \hat{x}_{i,3} + \phi_2(y, \dot{y}) + E_1 \lambda_{i,2} \text{sgn}(y_i - \hat{y}_i) \\ &\vdots \\ \dot{\hat{x}}_{i,\mu_i-1} &= \hat{x}_{i,\mu_i} + \phi_{\mu_i-1}(y, \dot{y}) + E_1 \lambda_{i,\mu_i-1} \text{sgn}(y_i - \hat{y}_i) \\ \dot{\hat{x}}_{i,\mu_i} &= \phi_{\mu_i}(y, \dot{y}) + E_1 \lambda_{i,\mu_i} \text{sgn}(y_i - \hat{y}_i) \\ \dot{\hat{y}}_i &= \hat{x}_{i,1} \end{aligned} \tag{4.10}$$

for  $i = 1, \dots, p$  where:  $\dot{\hat{y}}_i \triangleq \hat{x}_{i,2} + E_1 \lambda_{i,1} \text{sgn}(y_i - \hat{y}_i)$

From this, one deduces a part of the error's observation dynamic ( $e_{i,1} = (y_i - \hat{x}_{i,1})$  and  $e_{i,2} = \hat{y}_i - \hat{x}_{i,2}$ ):

$$\dot{e}_{i,1} = e_{i,2} + \lambda_{i,1} \text{sgn}(e_{i,1})$$

Therefore, using the same method as in the previous section one obtains:

**Theorem 38** *Under the conditions:*

- 1)  $\lambda_{i,1} > |e_{2,i}|_{\max}$  for  $i = 1, \dots, p$ .
- 2) All the  $\lambda_{i,j}$   $i = 1, \dots, p$ ,  $j = 2, \dots, \mu_i$  are such that  $\left[ sI - \left( A_i + \frac{\Lambda_i}{\lambda_{i,1}} u_1 \right) \right]$  is a Hurwitz polynomial. Where  $u_1 = (1, 0, \dots, 0)^T$  and  $A_i$  is the

$(\mu_i - 1) \times (\mu_i - 1)$  matrix defined by

$$A_i \text{ is a } \mathbb{R}^{(\mu_i-1) \times (\mu_i-1)} \text{ matrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & \ddots & 1 \\ 0 & 0 & 0 \end{pmatrix}$$

The observer (4.10) gives, in finite time  $t_0$ , the convergence of  $\hat{y}$  (respectively  $\dot{y}$ ) to  $y$  (respectively to  $\dot{y}$ ), and an asymptotic linear stable observation error dynamics on the sliding surface ( $e_{i,1} = 0$ ).

**Proof** The dynamics of the observation error are

$$\dot{e}_i = A_i e_i + \phi(y, \dot{y}) - \phi(y, \dot{\hat{y}}) - \Lambda_i \text{sgn}(y_i - \hat{y}_i)$$

for  $i = 1, \dots, p$ . It is clear that, after a finite time  $t_0$ , one has  $\dot{y} = \dot{\hat{y}}$ , so  $\phi(y, \dot{y}) - \phi(y, \dot{\hat{y}}) = 0$ . So that, for  $\forall t > t_0$  the error dynamics will be on the reduced manifold ( $e_{i,1} = 0$ ),  $\forall i \in \{1, \dots, p\}$ , and given by

$$\dot{\bar{e}}_i = A_i \bar{e}_i - \Lambda_i \frac{e_{i,2}}{\lambda_{i,1}} \quad \text{for } i = 1, \dots, p \quad (4.11)$$

with  $\bar{e}_i = (e_{i,2}, e_{i,3}, \dots, e_{i,\mu_i})$  which is linear. If  $\left[ sI - (A_i + \frac{\Lambda_i}{\lambda_{i,1}} u_1) \right]$  is Hurwitz, this dynamic is asymptotically stable.

One has shown that using a sliding mode observer (4.10), the system (4.9) may be, under an appropriate choice of  $\lambda_{i,j}$ , observed with a linear asymptotic stable observation error dynamics (4.11).

In the next proposition, one characterizes the observability indices of the output  $\bar{y} \triangleq (y, \dot{y}) = (h, L_f h)$ .

**Proposition 39** *Considering the system (4.8) with the extended output:  $\bar{y} = (y, \dot{y}) = (h, L_f h)$ :*

$$\begin{aligned} \dot{\xi} &= f(\xi) \\ \bar{y} &= (h(\xi), L_f h(\xi)) \end{aligned} \quad (4.12)$$

*the indices of observability become:*

$$\bar{\mu}_i = \begin{cases} 1 & \text{if } i \in \{1, \dots, p\} \\ & \text{one has } \bar{y}_i = y_j \text{ with } j = i \\ \mu_j - 1 & \text{if } i \in \{p+1, \dots, 2p\} \\ & \text{one has } \bar{y}_i = \dot{y}_j \text{ with } j = i - p \end{cases}$$

*where  $\mu_i$  is the observability indices of the output  $y_i$  in the system (4.8).*

For the proof see the appendix, page 123.

**Remark 40** *The necessary and sufficient conditions to obtain output and output derivative form are the same as those in Theorem 35 for the extended output  $\bar{y} = (y, \dot{y})$ .*

From the last remark, necessary and sufficient conditions for the existence of a diffeomorphism transforming (4.8) into (4.12) are given by applying Theorem 36 to system (4.12) rewritten only in terms of the real output  $y$ .

**Theorem 41** *There exists a change of coordinates transforming (4.12) into (4.9) if and only if*

1) *If one denotes (with a possible reordering of the  $h_i$ )*

$$Q = \left\{ L_f^{j-1}(dh_i) \text{ with } i = 1, \dots, p \text{ and } j = 1, \dots, \mu_i \right\}$$

*then  $\dim \text{span } Q = n$  in a neighborhood of  $\xi^0$ .*

2) *If one denotes for  $j = 1, \dots, p$*

$$Q_j = \left\{ L_f^{k-1}(dh_i) \begin{array}{l} i = 1, \dots, p \\ k = 1, \dots, \mu_j \end{array} \right\} - \left\{ L_f^{\mu_j-1}(dh_j) \right\}$$

*then for  $j = 1, \dots, p$   $\text{span } Q_j = \text{span } Q \cap Q_j$*

3) *There exists vector fields  $\bar{g}^1, \bar{g}^2, \dots, \bar{g}^{2p}$  satisfying:*

$$L_{\bar{g}^l} L_f^{l-1}(h_j) = \delta_{i,j} \delta_{l,\mu_i}, \quad \text{with } \begin{cases} i, j = 1, \dots, p, \\ l = 1, \dots, \mu_i \end{cases}$$

$$L_{\bar{g}^i}(h_j) = \delta_{i,j+p}, \quad \text{with } \begin{cases} i = p+1, \dots, 2p, \\ j = 1, \dots, p \end{cases}$$

$$\text{and } L_{\bar{g}^i}(L_f(h_j)) = 0, \quad \text{with } \begin{cases} i = p+1, \dots, 2p, \\ j = 1, \dots, p \end{cases}$$

4) *Setting :*

$$\bar{\Delta} = \left\{ \text{ad}_{(-f)}^k \bar{g}^i, \begin{array}{l} i = 1, \dots, p \\ k = 0, \dots, \mu_i - 2 \end{array} \right\} \cup \{ \bar{g}^i, i = p+1, \dots, 2p \}$$

$$\forall u, v \in \bar{\Delta}, \quad u \neq v \Rightarrow [u, v] = \mathbf{0}$$

For the proof see the appendix, page 124.

**Remark 42** *From the proof of Theorem 41, one can see that the Definition of  $\bar{g}^i$  for  $i = 1, \dots, p$  is the same as the definition of  $g^i$ . However, condition 3. is less restrictive than the one given in Theorem 35.*

**Example 43** *Let us consider the following system:*

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= x_3 + x_2^2 \\ \dot{x}_3 &= -x_3 - x_2 - x_1 \\ y &= x_1\end{aligned}\tag{4.13}$$

*which is in output and output derivative nonlinear injection form and can not be transformed into output injection form. In fact, as defined in Theorem 35, the vector  $g^1$  is such that:*

$$\begin{aligned}L_{g^1}(x_1) &= L_{g^1}(x_2) = 0 \\ L_{g^1}(x_3 + x_2^2) &= 1\end{aligned}\tag{4.14}$$

*So,  $g^1 = (0, 0, 1)^T$ ,  $ad_{(-f)}^1 g^1 = (0, 1, -1)^T$  and  $ad_{(-f)}^2 g^1 = (1, 2x_2 - 1, 0)^T$ .*

*The Lie brackets of these vectors are equal to*

$$\begin{aligned}\left[ g^1, ad_{(-f)}^1 g^1 \right] &= \left[ g^1, ad_{(-f)}^2 g^1 \right] = 0 \\ \left[ ad_{(-f)}^1 g^1, ad_{(-f)}^2 g^1 \right] &= (0, 2, 0)^T \neq 0\end{aligned}$$

*Consequently, this system does not verify the conditions of Theorem 35. Looking now at the conditions of Theorem 38, one has for the vectors  $\bar{g}^1$  and  $\bar{g}^2$ :*

$$\begin{aligned}L_{\bar{g}^1}(x_1) &= L_{\bar{g}^1}(x_2) = 0, \quad L_{\bar{g}^1}(x_3 + x_2^2) = 1 \\ L_{\bar{g}^2}(x_1) &= 1, \quad L_{\bar{g}^2}(x_2) = 0\end{aligned}$$

*So,  $\bar{g}^1 = (0, 0, 1)^T$ ,  $ad_{(-f)}^1 \bar{g}^1 = (0, 1, -1)^T$ , and  $\bar{g}^2 = (1, 0, *)^T$ . Then if one chooses  $* = 0$  for example, one obtains:*

$$\left[ \bar{g}^1, ad_{(-f)}^1 \bar{g}^1 \right] = \left[ \bar{g}^2, \bar{g}^1 \right] = \left[ \bar{g}^2, ad_{(-f)}^1 \bar{g}^1 \right] = 0$$

*Thus, this system verifies all the conditions of Theorem 38. Choosing  $z_1 = x_1$ ;  $z_2 = x_2$ ;  $z_3 = x_2 + x_3$ , one obtains in the new coordinates the following system:*

$$\begin{aligned}\dot{z}_1 &= z_2 \\ \dot{z}_2 &= z_3 + \phi_2(z_1, z_2) \\ \dot{z}_3 &= \phi_3(z_1, z_2) \\ y &= z_1\end{aligned}$$

**Remark 44** Every system in the form of (4.6) is obviously on the form (4.9). One important consequence of the previous remark and the example is that the conditions of Theorem 35 imply conditions of Theorem 38, but the converse is false.

In the next section we consider an actuated system but for the sake of simplicity only in a single input single output (SISO) form.

## 4.4 Triangular input observer form

Let us consider the following SISO analytic system  $\Sigma$

$$\begin{aligned}\dot{x} &= f(x) + g(x, u) \\ y &= h(x)\end{aligned}\tag{4.15}$$

where  $x \in \mathbb{R}^n$  is the state,  $u \in \mathbb{R}$  is the input,  $y \in \mathbb{R}$  is the output and  $f, g, h$  are analytical function vectors of appropriate dimensions. Moreover for any  $x \in \mathbb{R}^n$  the function  $g(x, 0)$  is equal to zero and the system (4.15) is assumed bounded input bounded state in finite time. In order to transform (4.15) in a triangular input observer form, we modified the classical *observation rank condition*:

**Condition 45**

$$\text{rank} \begin{pmatrix} dh \\ dL_f h \\ \vdots \\ dL_f^{n-1} h \\ dL_f^\infty h \end{pmatrix} = n$$

where  $L_f$  denotes the classical Lie derivative in  $f$  and  $dh$  is the classical one form.

**Remark 46** Condition 45 is the classical one for an autonomous system. In the nonlinear context, we can't refer to the Cayley–Hamilton theorem.

But in the next we assume

**Condition 47**

$$\text{rank} \begin{pmatrix} dh \\ dL_f h \\ \vdots \\ dL_f^{n-1} h \end{pmatrix} = n$$

From condition 47 it is known that the codistribution

$$\Omega^i = \text{span}\{dh, \dots, dL_f^i h\} \quad 0 \leq i \leq n-1$$

is involutive. We also need the following condition

**Condition 48** *The vector field  $g$  verifies for any  $u \in \mathbb{R}$*

$$dL_g L_f^i h \in \Omega^i \quad \forall i \in \{0, \dots, n-1\}$$

Now we can set the following Theorem :

**Theorem 49** *System (4.15) may be transformed, by diffeomorphism, in the neighborhood of  $x$  in a triangular input observer form*

$$\begin{pmatrix} \dot{\xi}_1 \\ \dot{\xi}_2 \\ \vdots \\ \dot{\xi}_{n-1} \\ \dot{\xi}_n \end{pmatrix} = \begin{pmatrix} \xi_2 + \bar{g}_1(\xi_1, u) \\ \xi_3 + \bar{g}_2(\xi_1, \xi_2, u) \\ \vdots \\ \xi_n + \bar{g}_{n-1}(\xi_1, \dots, \xi_{n-1}, u) \\ f_n(\xi) + \bar{g}_n(\xi, u) \end{pmatrix} \quad (4.16)$$

$$y = \xi_1$$

with  $\bar{g}_i(\cdot, u=0) = 0$  for any  $i \in \{1, \dots, n\}$ , if and only if conditions 47 and 48 hold in the neighborhood of  $x$ .

For the proof see the appendix, page 125.

#### 4.4.1 Sliding mode observer design for triangular input observer form

From the work of Drakunov and Utkin [14, 15] and our previous work [28, 16, 6], we propose the *sliding observer for triangular input observer form*

$$\begin{pmatrix} \dot{\hat{\xi}}_1 \\ \dot{\hat{\xi}}_2 \\ \vdots \\ \dot{\hat{\xi}}_{n-1} \\ \dot{\hat{\xi}}_n \end{pmatrix} = \begin{pmatrix} \hat{\xi}_2 + \bar{g}_1(\xi_1, u) + \lambda_1 \text{sgn}(\xi_1 - \hat{\xi}_1) \\ \hat{\xi}_3 + \bar{g}_2(\xi_1, \tilde{\xi}_2, u) + \lambda_2 \text{sgn}_1(\tilde{\xi}_2 - \hat{\xi}_2) \\ \vdots \\ \hat{\xi}_n + \bar{g}_{n-1}(\xi_1, \tilde{\xi}_2, \dots, \tilde{\xi}_{n-1}, u) + \lambda_{n-1} \text{sgn}_{n-2}(\tilde{\xi}_{n-1} - \hat{\xi}_{n-1}) \\ f_n(\xi_1, \tilde{\xi}_2, \dots, \tilde{\xi}_n) + \bar{g}_n(\xi_1, \tilde{\xi}_2, \dots, \tilde{\xi}_n, u) + \lambda_n \text{sgn}_{n-1}(\tilde{\xi}_{n-1} - \hat{\xi}_n) \end{pmatrix} \quad (4.17)$$

where

$$\begin{aligned}\tilde{\xi}_2 &= \hat{\xi}_2 + \lambda_1 \text{sgn}_1(\xi_1 - \hat{\xi}_1) \\ \tilde{\xi}_3 &= \hat{\xi}_3 + \lambda_2 \text{sgn}_2(\tilde{\xi}_2 - \hat{\xi}_2) \\ &\vdots \\ \tilde{\xi}_n &= \hat{\xi}_n + \lambda_n \text{sgn}_{n-1}(\tilde{\xi}_{n-1} - \hat{\xi}_{n-1})\end{aligned}$$

and the  $\text{sgn}_i(\xi)$  function denotes the usual sgn function but with a low pass filter of the  $\xi$  variable [15] and an anti-peaking structure [6]. This anti-peaking structure follows the idea that we do not inject the observation error information before reaching the sliding manifold linked with this information (i.e.,  $\text{sign}_i = E_i \text{sign}$ , with  $E_i = 1$  if  $E_1 = \dots = E_{i-1} = 1$  and  $\xi_1 - \hat{\xi}_1 = 0$  else  $E_i = 0$ ). Moreover we reach the manifold one by one. Doing this we obtain a “high gain” dynamic (i.e., see the equivalence between the sliding mode and the high gain [32]) of dimension one and consequently we do not have a peaking phenomena [42]. More precisely  $\text{sgn}_i(\cdot)$  is equal to zero if there exists  $0 < j < i - 1$  such that  $\tilde{\xi}_j - \hat{\xi}_j \neq 0$  (by definition  $\tilde{\xi}_1 = \xi_1$ ), else  $\text{sgn}_i(\cdot)$  is equal to the usual  $\text{sgn}(\cdot)$  function. In the observer structure, this particular  $\text{sgn}$  function allows that  $\tilde{\xi}_i - \hat{\xi}_i$  converges to zero if all the  $\tilde{\xi}_j - \hat{\xi}_j$  with  $j < i$  have converged to zero before.

**Theorem 50** *Considering a bounded input bounded state (BIBS) in finite time system (4.16) and observer (4.17), for any initial state  $\xi(0)$ ,  $\hat{\xi}(0)$  and any bounded input  $u$ , there exists a choice of  $\lambda_i$  such that the observer state  $\hat{\xi}$  converges in finite time to  $\xi$ .*

**Proof** From (4.16) and (4.17) and considering the initial state condition such that  $\xi_1(0) \neq \hat{\xi}_1(0)$  (if this is not the case, we directly move on to the next step of the proof). Thus we are in the

• **first step** of our proof and we obtain the following observation error dynamics  $e = \xi - \hat{\xi}$ .

$$\begin{pmatrix} \dot{e}_1 \\ \dot{e}_2 \\ \vdots \\ \dot{e}_{n-1} \\ \dot{e}_n \end{pmatrix} = \begin{pmatrix} e_2 - \lambda_1 \text{sgn}(\xi_1 - \hat{\xi}_1) \\ e_3 + \bar{g}_2(\xi_1, \xi_2, u) - \bar{g}_2(\xi_1, \hat{\xi}_2, u) \\ \vdots \\ e_n + \bar{g}_{n-1}(\xi_1, \xi_2, \dots, \xi_{n-1}, u) - \bar{g}_{n-1}(\xi_1, \hat{\xi}_2, \dots, \hat{\xi}_{n-1}, u) \\ (\bar{f}_n(\xi) - \bar{f}_n(\xi_1, \hat{\xi}_2, \dots, \hat{\xi}_n) + \bar{g}_n(\xi, u) - \bar{g}_n(\xi_1, \hat{\xi}_2, \dots, \hat{\xi}_n, u)) \end{pmatrix}$$

Thus as the input  $u$  is bounded the state  $\xi$  does not go to infinity in finite time. Moreover if  $\hat{\xi}_1$  is bounded all the states of the observer are also

bounded during step 1. Consequently the observation error state is also bounded. Now, setting  $V_1 = \frac{e_1^2}{2}$ , we have

$$\dot{V}_1 = e_1(e_2 - \lambda_1 \operatorname{sgn}(e_1))$$

Thus choosing  $\lambda_1 > |e_2|_{max}$  the observation error  $e_1$  goes to zero in finite time  $t_1$ . Moreover, if after  $t_1$  the observation error stays equal to zero (i.e.,  $\lambda_1 > |e_2|_{max}$ ) we have  $e_2 = \lambda_1 \operatorname{sgn}(\xi_1 - \hat{\xi}_1)$  and consequently  $\tilde{\xi}_2 = \xi_2$ . Now we pass to the:

• **second step.** Here, we ensure that the observation error  $e_2$  is bounded in order to remain on the manifold  $e_1 = 0$ . Moreover, we want to reach the submanifold  $e_1 = e_2 = 0$ . Using the same argument as in [14, 15] the equivalent vector is obtained in finite time via a low pass filtering of  $\lambda_1 \operatorname{sgn}(\xi_1 - \hat{\xi}_1)$  which is equal to  $e_2$ . Thus, as at  $t_1$ , we have  $e_1 = 0$ , and the observation error is now equal to

$$\begin{pmatrix} \dot{e}_1 \\ \dot{e}_2 \\ \dot{e}_3 \\ \vdots \\ \dot{e}_{n-1} \\ \dot{e}_n \end{pmatrix} = \begin{pmatrix} e_2 - \lambda_1 \operatorname{sgn}(\xi_1 - \hat{\xi}_1) = 0 \\ e_3 - \lambda_2 \operatorname{sgn}(\xi_2 - \hat{\xi}_2) \\ e_4 + \bar{g}_3(\xi_1, \xi_2, \xi_3, u) - \bar{g}_3(\xi_1, \xi_2, \hat{\xi}_3, u) \\ \vdots \\ e_n + \bar{g}_{n-1}(\xi_1, \xi_2, \dots, \xi_{n-1}, u) - \bar{g}_{n-1}(\xi_1, \xi_2, \hat{\xi}_3, \dots, \hat{\xi}_{n-1}, u) \\ (\bar{f}_n(\xi) - \bar{f}_n(\xi_1, \xi_2, \dots, \hat{\xi}_n) + \bar{g}_n(\xi, u) - \bar{g}_n(\xi_1, \xi_2, \dots, \hat{\xi}_n, u)) \end{pmatrix}$$

Setting  $V_2 = \frac{e_1^2}{2} + \frac{e_2^2}{2}$ , we obtain

$$\dot{V}_2 = e_1(e_2 - \lambda_1 \operatorname{sgn}(e_1)) + e_2(e_3 - \lambda_2 \operatorname{sgn}(e_2))$$

Moreover, if the condition  $\lambda_1 > |e_2|_{max}$  holds for  $t > t_1$ , we have  $e_1 = 0$  and  $e_2 - \lambda_1 \operatorname{sgn}(e_1) = 0$ , thus we find

$$\dot{V}_2 = e_2(e_3 - \lambda_2 \operatorname{sgn}(e_2))$$

Consequently  $e_2$  goes to zero in finite time  $t_2 > t_1$  if  $\lambda_2 > |e_3|_{max}$ . Moreover, from  $V_2$  we obtain that the observation error is strictly decreasing during the period of time  $[t_1, t_2]$ . This implies that the condition on  $\lambda_1$  is verified after  $t_1$  if it is verified before  $t_1$ . Moreover as the input is bounded, the state  $\xi$  stays bounded during the period  $[0, t_2]$  and from the structure of the observation error the dynamics  $e$  is also bounded and consequently  $\hat{\xi}$  is too.

Now let us assume that we are at the step  $j < n$ . This step starts at time  $t_{j-1}$  and at  $t_{j-1}$ , all the  $e_k = 0$  and all the conditions on  $\lambda_k$  are

verified for  $k < j$ . Thus, we proceed to

• **step  $j$** . The observation error dynamic is equal to

$$\begin{pmatrix} \dot{e}_1 \\ \vdots \\ \dot{e}_{j-1} \\ \dot{e}_j \\ \dot{e}_{j+1} \\ \vdots \\ \dot{e}_{n-1} \\ \dot{e}_n \end{pmatrix} = \begin{pmatrix} e_2 - \lambda_1 \operatorname{sgn}(\xi_1 - \hat{\xi}_1) = 0 \\ \vdots \\ e_j - \lambda_{j-1} \operatorname{sgn}(\xi_{j-1} - \hat{\xi}_{j-1}) = 0 \\ e_{j+1} + \lambda_j \operatorname{sgn}(\xi_j - \hat{\xi}_j) \\ e_{j+2} + \bar{g}_{j+1}(\xi_1, \dots, \xi_{j+1}, u) - \bar{g}_{j+1}(\xi_1, \dots, \xi_j, \hat{\xi}_{j+1}, u) \\ \vdots \\ e_n + \bar{g}_{n-1}(\xi_1, \xi_2, \dots, \xi_{n-1}, u) \\ -\bar{g}_{n-1}(\xi_1, \dots, \xi_j, \hat{\xi}_{j+1}, \dots, \hat{\xi}_{n-1}, u) \\ (\bar{f}_n(\xi) - \bar{f}_n(\xi_1, \dots, \xi_j, \hat{\xi}_{j+1}, \dots, \hat{\xi}_n)) \\ + \bar{g}_n(\xi, u) - \bar{g}_n(\xi_1, \dots, \xi_j, \hat{\xi}_{j+1}, \dots, \hat{\xi}_n, u) \end{pmatrix}$$

Setting  $V_j = \sum_{i=1}^j \frac{e_i^2}{2}$  we deduce from  $e_k = 0 \forall i < j$  that

$$\dot{V}_j = e_j(e_{j+1} - \lambda_j \operatorname{sgn}(e_j))$$

Consequently  $e_j$  goes to zero in finite time  $t_j > t_{j-1}$  if  $\lambda_j > |e_{j+1}|_{\max}$  and all  $\lambda_k$  conditions are verified for  $k < j$ . As the input is bounded  $\xi$  is bounded and from the observer structure  $\hat{\xi}_j$  is also bounded during the period  $[0, t_j]$ . It follows that  $e_j$  is bounded and we can find  $\lambda_j$  such that  $\lambda_j > |e_{j+1}|_{\max}$  is verified. Moreover, as  $e_j$  is decreasing during the period  $[t_{j-1}, t_j]$ ,  $\lambda_{j-1} > |e_j|_{\max}$  is verified during this period and therefore all the  $e_k$  remain equal to zero for any  $k < j$ .

Now we go to :

• **step  $n$** . This step starts at the time  $t_{n-1}$  and at this time  $e_k = 0$  for any  $k < n$ . Thus we obtain the following observation error dynamics

$$\begin{pmatrix} \dot{e}_1 \\ \vdots \\ \dot{e}_{n-1} \\ \dot{e}_n \end{pmatrix} = \begin{pmatrix} e_2 + \lambda_1 \operatorname{sgn}(\xi_1 - \hat{\xi}_1) = 0 \\ \vdots \\ e_n + \lambda_{n-1} \operatorname{sgn}(\xi_{n-1} - \hat{\xi}_{n-1}) = 0 \\ \lambda_n \operatorname{sgn}(\xi_n - \hat{\xi}_n) \end{pmatrix}$$

Setting  $V_n = \sum_{i=1}^n \frac{e_i^2}{2}$  we deduce from  $e_k = 0 \forall i < n$  that

$$\dot{V}_n = e_n [-\lambda_n \operatorname{sgn}(e_n)]$$

So,  $e_n$  go to zero in finite time  $t_n > t_{n-1}$  for any  $\lambda_n > 0$  and if all the conditions on the  $\lambda_k$  for  $k < n$  are verified after  $t_{n-1}$ . Condition on  $\lambda_{n-1}$  is always verified because  $e_n$  is decreasing after  $t_{n-1}$  and by induction all conditions follow.

#### 4.4.2 Observer matching condition

It is well known from the work [19] that roughly speaking, a condition in order to reject a perturbation, is that the perturbation act in the same direction of the control.

In the same manner of thinking, for observer design we obtain the condition in order to observe the state under unknown perturbation. Consider the linear observable bounded perturbed system:

$$\dot{x} = Ax + Bu + Pw \quad (4.18)$$

and the output equation is  $y = Cx$  with  $y \in \mathbb{R}$ ,  $x \in \mathbb{R}^n$ ,  $u \in \mathbb{R}^m$  and  $w \in [-B_w, B_w]$

$$\mathcal{O}(A, C) = \begin{pmatrix} C \\ \vdots \\ CA^{n-2} \end{pmatrix} = n$$

A condition in order to cancel the perturbation effect on the state observation is that

$$\begin{pmatrix} C \\ \vdots \\ CA^{n-2} \end{pmatrix} P = 0$$

which is called the *observer matching condition*.

**Remark 51** *Necessity is obvious such that the perturbation derivative time does not act on the state observations.*

Sufficiency is clear: considering for example, an observer for triangular input observer.

Generalizing the previous observer matching condition to the bounded input bounded state single input single output (BIBS-SISO) local weakly observable nonlinear perturbed system:

$$\begin{aligned} \dot{x} &= f(x) + g(x)u + p(x)w := F(x, u) + p(x)w \\ y &= h(x) \end{aligned} \quad (4.19)$$

where  $x \in \mathbb{R}^n$ ,  $u \in \mathbb{R}^m$ , and the bounded perturbation  $w \in [-B_w, B_w]$ , and  $f$ ,  $g$ ,  $p$  are functions vector fields of appropriate dimensions.

We immediately obtain the following sufficient conditions in order to reject the perturbation effect on the observer.

**Proposition 52** *If the system (4.19) without perturbation verifies conditions (47) and Condition 48 of Theorem 49 and the observer matching condition*

$$\begin{pmatrix} dh \\ dL_F h \\ \vdots \\ dL_F^{n-2} h \end{pmatrix} p(x) = 0 \quad (4.20)$$

*in the neighborhood of  $x$ , and where the Lie derivative is done with respect to  $x$  and  $u$ . Then it is possible to locally design an observer which estimates all state components and does this in both cases: with and without perturbation.*

**Proof** The proof is a direct consequence of Theorem 49 and sliding mode triangular observer design.

## 4.5 Simulations and comments

Let us consider the following system  $\Sigma$  which is in the triangular input observer form

$$\begin{aligned} \dot{x}_1 &= x_2 - x_1^3 u \\ \dot{x}_2 &= x_3 + x_2 x_1 u \\ \dot{x}_3 &= -3x_3 - 3x_2 - x_1 - x_3^3 - u \\ y &= x_1 \end{aligned} \quad (4.21)$$

For this system, the observer 4.17 takes the form

$$\begin{aligned} \dot{\hat{x}}_1 &= \hat{x}_2 - \hat{x}_1^3 u + \lambda_1 \operatorname{sgn}(x_1 - \hat{x}_1) \\ \dot{\hat{x}}_2 &= \hat{x}_3 + \tilde{x}_2 x_1 u + \lambda_2 \operatorname{sgn}_1(\tilde{x}_2 - \hat{x}_2) \end{aligned} \quad (4.22)$$

$$\begin{aligned} \dot{\hat{x}}_3 &= -3\tilde{x}_3 - 3\tilde{x}_2 - x_1 - \tilde{x}_3^3 - u + \lambda_3 \operatorname{sgn}_2(\tilde{x}_3 - \hat{x}_3) \\ y &= x_1 \end{aligned} \quad (4.23)$$

with  $\tilde{x}_2 = \hat{x}_2 + \lambda_1 \operatorname{sgn}_1(x_1 - \hat{x}_1)$  and  $\tilde{x}_3 = \hat{x}_3 + \lambda_2 \operatorname{sgn}_2(\tilde{x}_2 - \hat{x}_2)$ , and where  $\operatorname{sgn}_i$  functions are designed as noted in Section 4.3.

This approach has been tested by simulation with the following initial conditions  $x = (1, 0.5, 0.5)^T$  and  $\hat{x} = (0, 0, 0)^T$ . Moreover, we have chosen a first-order low pass filter with a cut frequency equal to 100Hz and observation gain  $\lambda_1$ ,  $\lambda_2$ , and  $\lambda_3$  respectively equal to 4, 2, and 2. Moreover the function “ $\operatorname{sgn}$ ” is approximated by a saturation function with a slow rate equal to  $10^4$ .

In Figure 4.1, we see that  $\hat{x}_1$  reaches  $x_1$  in finite time  $\simeq 0.25s$ . In Figure 4.2, we see that  $\hat{x}_2$  also reaches  $x_2$  in finite time  $\simeq 0.75s$ . But  $\hat{x}_2$  will only reach  $x_2$  when  $\hat{x}_1$  will be equal to  $x_1$ . In Figure 4.3, we see that  $\hat{x}_3$  reaches  $x_3$  in finite time  $\simeq 1s$ .

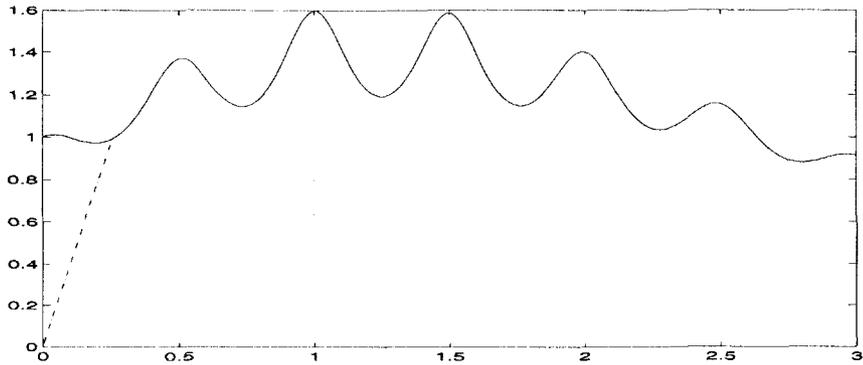


Figure 4.1:  $x_1(-)$  and  $\hat{x}_1(-)$

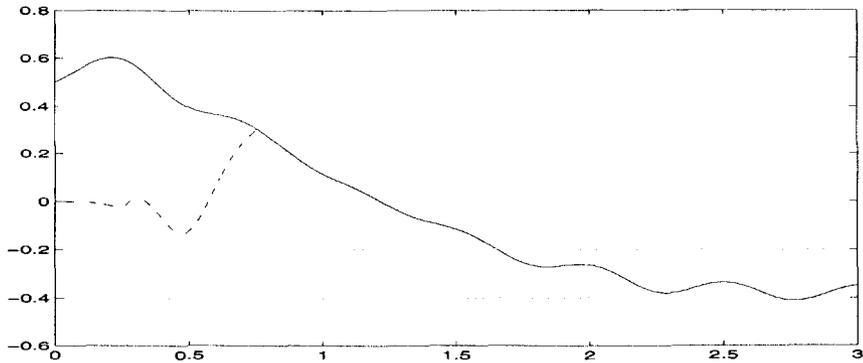


Figure 4.2:  $x_2(-)$  and  $\hat{x}_2(-)$

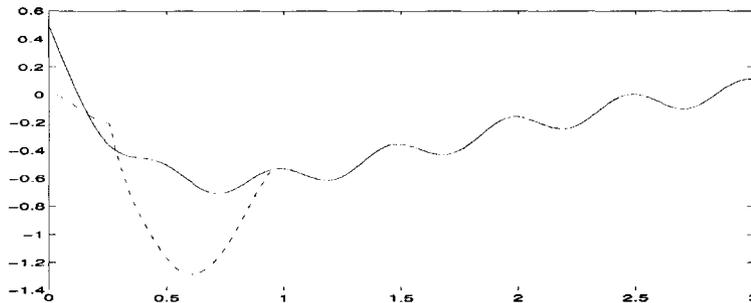


Figure 4.3:  $x_3(-)$  and  $\hat{x}_3 (-)$

Now, starting from the same initial conditions, we add an output noise in order to show the behavior of the observer in this case. In [6], following the work of Yaz and Azemi [47], the author proposed to use a saturation function with dead zone for observer in the case of the extended injection form. This reduces the observer sensitivity to the noise, but we were obliged to change the observer gain as follows  $\lambda_1 = \lambda_2 = \lambda_3 = 4$  in order to recover a time response quite similar to the previous simulation.

In Figures 4.4, 4.5, 4.6 and 4.7, we see that the observer state  $\hat{x}$  reaches the neighborhood of the system state  $x$  in finite time. But we also see that the noise is not totally suppressed in the observer. We can reduce this noise with some minor modifications by introducing an asymptotic gain or a *sgn* function modified with respect to the noise output knowledge [47], for example.

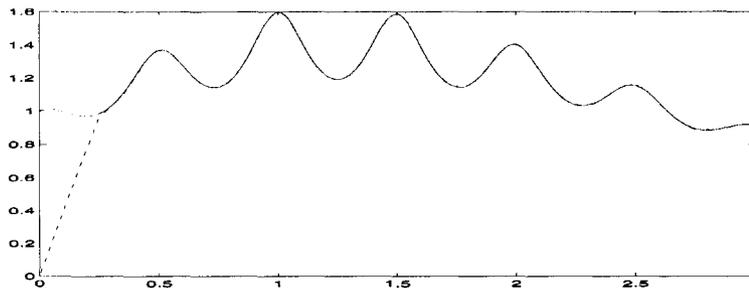


Figure 4.4:  $x_1(-)$  and  $\hat{x}_1 (-)$

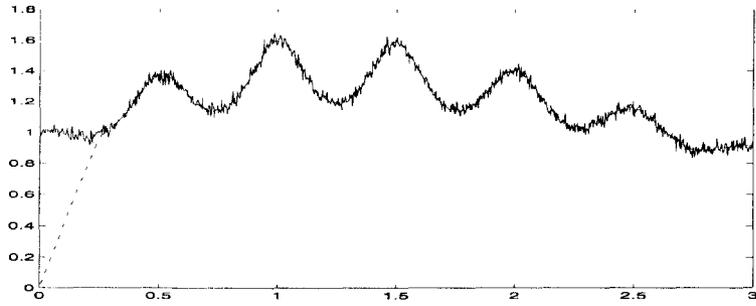


Figure 4.5: Measured  $x_1(-)$  and  $\hat{x}_1(-)$

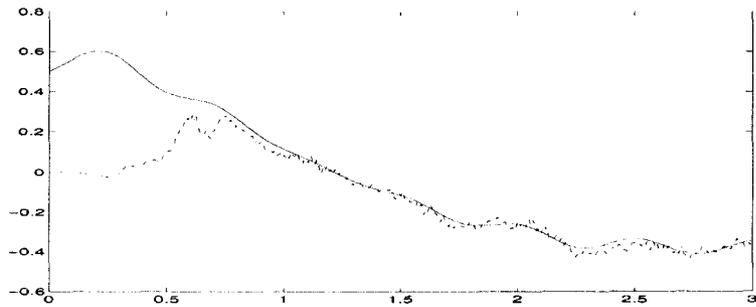


Figure 4.6:  $x_2(-)$  and  $\hat{x}_2(-)$

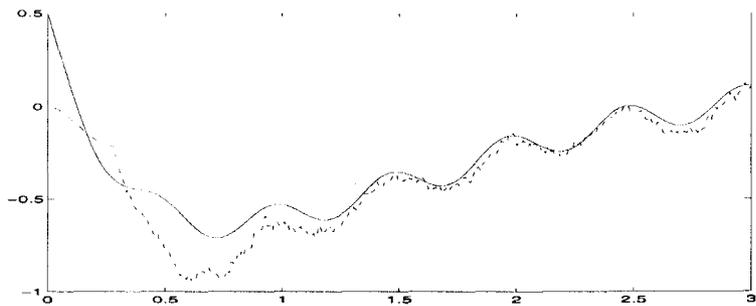


Figure 4.7:  $x_3(-)$  and  $\hat{x}_3(-)$

## 4.6 Conclusion

In this chapter, we introduced a sliding observer that does not depend on the derivative of  $u$ . This is due to the fact that our main application domain is the AC motor where the derivative of the input does not exist or is not easy to obtain. This appears, for example, when we consider the converter in the observer and control scheme. But, if it exists, and if it is technologically possible to obtain  $\dot{u}$ ,  $\ddot{u}$ , ..., and so on. A very clever observer form was given in [23]. For this form, many observer designs work well, and in this case, advantages of the sliding mode observer were principally the design simplicity and the finite time convergence. In practical observer design, we always take into account the output noise, thus generally we replace the  $sgn$  function by a modified  $sgn$  function or higher order sliding mode. In the latter, we think that it is important, when it is possible, as it is proposed in [15], to design an observer without the use of diffeomorphism, because the observer validity domain is restricted to the diffeomorphism validity domain.

## 4.7 Appendix

### 4.7.1 Proof of Proposition 39

From Definition 33, the indices  $\mu_i$  verify:

- $\sum_{i=1}^p \mu_i = n$ , so from the Definition of  $\bar{\mu}_i$ , one has:  $\sum_{i=1}^{2p} \bar{\mu}_i = n$ .

- $\Delta = \left\{ L_f^{j-1}(dh_i) : i = 1, \dots, p; j = 1, \dots, \mu_i \right\}$  are linearly independent.

As  $L_f^j(dh_i) = L_f^{j-1}(L_f(dh_i)) = L_f^{j-1}(\dot{y}_i)$ .  $\Delta$  will be rewritten as

$$\left\{ L_f^{j-1}(d\bar{y}_i) : i = 1, \dots, 2p; j = 1, \dots, \bar{\mu}_i \right\}$$

- Thus, if  $\mu_i$  verify 3. of Definition 33, it is easy to see that: If  $l_1, \dots, l_{2p}$  satisfies  $\sum_{i=1}^{2p} l_i = n$  and  $\left\{ L_f^{j-1}(d\bar{y}_i) : i = 1, \dots, 2p; j = 1, \dots, l_i \right\}$  are linearly independent at some  $\xi \in \mathcal{U}$ , then  $(l_1, \dots, l_{2p}) \geq (\bar{\mu}_1, \dots, \bar{\mu}_{2p})$  in the lexicographic reordering  $[(l_1 > \bar{\mu}_1) \text{ or } (l_1 = \bar{\mu}_1 \text{ and } l_2 > \bar{\mu}_2) \text{ or } \dots \text{ or } (l_1 = \bar{\mu}_1, \dots, l_p = \bar{\mu}_{2p})]$ .

Then, the  $2p$ -tuple  $\bar{\mu}_1, \dots, \bar{\mu}_{2p}$  satisfies the three conditions of Definition 33.

## 4.7.2 Proof of Theorem 41

First, starting from Theorem 36, where  $y$  is substituted by  $\bar{y}$ , one proves hereafter that conditions 1. and 2. of Theorem 35 (which are required in Theorem 36) are equivalent to conditions 1. and 2. of Theorem 41. For the Theorem 36, let us define:  $\bar{Q} = \left\{ L_f^{j-1}(d\bar{y}_i) : i = 1, \dots, 2p; j = 1, \dots, \bar{\mu}_i \right\}$

and for  $j = 1, \dots, 2p$   $\bar{Q}_j = \left\{ L_f^{k-1}(d\bar{y}_i) : \begin{array}{l} i = 1, \dots, 2p; \\ k = 1, \dots, \bar{\mu}_j \end{array} \right\} - \left\{ L_f^{\bar{\mu}_j-1}(d\bar{y}_j) \right\}$

but

$\bar{Q} = \left\{ L_f^{j-1}(L_f(dh_i)) : \begin{array}{l} i = 1, \dots, p; \\ j = 1, \dots, \mu_i - 1 \end{array} \right\} \cup \{h_1, \dots, h_p\}$  and  $L_f^{j-1}(L_f(dh_i)) = L_f^j(dh_i)$ , then:

$$\bar{Q} = Q$$

So the equivalence of condition 1. is proved. Now, for condition 2., for Theorem 36 one computes  $\bar{Q}_j$ .

• For  $j = 1, \dots, p$  one has:

$$\bar{Q}_j = \left\{ L_f^{k-1}[L_f(d\bar{y}_i)] : \begin{array}{l} i = 1, \dots, 2p; \\ k = 1, \dots, \bar{\mu}_j - 1 \end{array} \right\}$$

and  $\bar{y}_j = L_f(h_j)$ , so

$$\bar{Q}_j = \left\{ \left[ L_f^{k-1}(L_f(dh_i)) : \begin{array}{l} i = 1, \dots, p; \\ k = 1, \dots, \mu_j - 1 \end{array} \right] \cup \{h_1, \dots, h_p\} \right\} - \left\{ L_f^{\mu_j-1-1}(L_f(dh_j)) \right\}$$

as  $L_f^k(L_f(d\bar{y}_{i+p})) = L_f^{k-1}[L_f(d\bar{y}_i)]$ , one immediately has  $\bar{Q}_j = Q_j$ .

• For  $j = p+1, \dots, 2p$  one has  $\bar{y}_j = h_j$ , so

$\bar{Q}_j = \{dh_1, dh_2, \dots, dh_p, L_f(dh_1), \dots, L_f(dh_p)\} - \{dh_j\}$  then, as  $\mu_i \geq 2$ , one obtains  $\bar{Q}_j \cap Q = Q_j$  for  $j = 1, \dots, p$ .

Thus, the condition 2. of Theorem 41 is equivalent to condition 2. of Theorem 35.

Secondly, in the same way, one proves the equivalence between conditions 3. and 4. of Theorem 41, and the last conditions of Theorem 36, where  $y$  is substituted by  $\bar{y}$ . Theorem 36 applied to  $\bar{y}$  gives:

There exists a change of coordinates transforming (4.12) into (4.9) if and only if the previous conditions hold and there exist vector fields  $\bar{g}^1, \bar{g}^2, \dots, \bar{g}^{2p}$  satisfying

$$L_{\bar{g}^i} L_f^{l-1}(\bar{y}_j) = \delta_{i,j} \delta_{l, \bar{\mu}_i}, \quad \begin{array}{l} i, j = 1, \dots, 2p, \\ l = 1, \dots, \bar{\mu}_i, \end{array}$$

such that

$$[ad_{(-f)}^k \bar{g}^i, ad_{(-f)}^l \bar{g}^j] = 0 \quad (4.24)$$

for  $i, j = 1, \dots, 2p$ ;  $k = 0, \dots, \bar{\mu}_i - 1$ ;  $l = 0, \dots, \bar{\mu}_j - 1$ .

Now, one wants to rewrite this condition only as a function of  $y$ . Therefore, the  $p$  first vector fields  $\bar{g}^i$  are defined such that

$$L_{\bar{g}^i} L_f^{l-1}(\bar{y}_j) = \delta_{i,j} \delta_{l, \mu_i - 1}, \quad \begin{array}{l} i = 1, \dots, p, \quad j = 1, \dots, 2p \\ l = 1, \dots, \mu_i - 1, \end{array}$$

with the Definition of  $\bar{y}_j$ , this is equivalent to the real output  $y$  to

$$L_{\bar{g}^i} L_f^{l-1}(y_j) = \delta_{i,j} \delta_{l, \mu_i}, \quad \begin{array}{l} i, p = 1, \dots, p, \\ l = 1, \dots, \mu_i, \end{array} \quad (4.25)$$

Now, the  $p$ -last vector fields  $\bar{g}^i$  are defined such that

$$L_{\bar{g}^i}(\bar{y}_j) = \delta_{i,j}, \quad \begin{array}{l} i = p + 1, \dots, 2p, \\ j = 1, \dots, 2p \end{array}$$

which can be rewritten as:

$$\begin{array}{l} L_{\bar{g}^i}(h_j) = \delta_{i,j}, \quad i = p + 1, \dots, 2p, \\ L_{\bar{g}^i}(L_f(h_j)) = 0, \quad j = 1, \dots, p \end{array} \quad (4.26)$$

Thus, from (4.25) and (4.26), one obtains condition 3. of Theorem 41. Moreover, from this and (4.24) one immediately finds condition 4. of Theorem 41 and reciprocally.

### 4.7.3 Proof of Theorem 49

#### Sufficiency

If condition 47 holds, then

$$\begin{pmatrix} \xi_1 \\ \xi_2 \\ \vdots \\ \xi_n \end{pmatrix} = \begin{pmatrix} h \\ L_f(h) \\ \vdots \\ l_f^{n-1} h \end{pmatrix}$$

is a diffeomorphism and transforms system (4.15) in

$$\begin{pmatrix} \dot{\xi}_1 \\ \dot{\xi}_2 \\ \vdots \\ \dot{\xi}_{n-1} \\ \dot{\xi}_n \end{pmatrix} = \begin{pmatrix} \xi_2 + \bar{g}_1(\xi, u) \\ \xi_3 + \bar{g}_2(\xi, u) \\ \vdots \\ \xi_n + \bar{g}_{n-1}(\xi, u) \\ f_n(\xi) + \bar{g}_n(\xi, u) \end{pmatrix}$$

with  $\bar{g}_i(\xi, u = 0) = 0$  for any  $i \in \{1, \dots, n\}$ . Moreover, in the  $x$  coordinate, condition 48 is equal to

$$d\bar{g}_i \in \text{span}\{dx_1, \dots, dx_i\} \quad \forall i \in \{1, n\} \quad (4.27)$$

this implies that the system is in form 4.16.

### Necessity

If there exists a diffeomorphism  $\xi = \phi(x)$  which transforms (4.15) into (4.16) condition 47 is directly verified by the existence of  $\phi$ . Moreover as (4.27) is a necessary condition, this implies that condition 48 is a necessary condition too.

## References

- [1] J-P. Barbot, T. Boukhobza and M. Djemai, "Triangular input observer form and sliding mode observer", *IEEE CDC 96*, pp 1489–1491, 1996.
- [2] J-P. Barbot, M. Djemai, T. Boukhobza and A. Glumineau, "Observateurs nonlinéaires de type mode glissants: Application à la machine asynchrone", *Commande des Machines Asynchrones*, Vol II, Optimisation, Discrétisation et Observateurs, C. Canudas de Wit, Ed. Hermès, pp. 223–294, 2000.
- [3] G. Bartolini and A. Ferrara, "Real-time output derivatives estimation by means of higher order sliding modes", in *proc. CESA 98*, Tunisia, 1998.
- [4] G. Bartolini and T. Zolezzi, "Control of nonlinear variable structure systems", *Journal of Math. Anal Appl.*, Vol. 15, No. 1, pp 42–62, 1986.
- [5] A.M. Bloch and Drakunov, S., "Stabilization and tracking in the non-holonomic integrator via sliding mode", *Syst. Contr. Lett.*, Vol. 29, No. 2, pp.91–99, 1996.
- [6] T. Boukhobza, "Contribution aux formes d'observabilité pour les observateurs à modes glissants et étude des commandes par ordres supérieurs", *Thèse de Doctorat*, Université de Paris Sud, Orsay, 1997.
- [7] T. Boukhobza and J-P. Barbot, "High order sliding mode observer", in *Proc IEEE-CDC98*, Tampa, 1998.
- [8] D. Bestle and M. Zeitz, "Canonical form observer design for nonlinear time varying systems", *Int. J. of Control*, Vol. 38, pp 429–431, 1983.

- [9] J. Birk and M. Zeitz, "Extended Luenberger observers for nonlinear multivariable systems", *Int. J. of Control*, Vol. 47, pp 1823–1836, 1988.
- [10] K. Busawon H. Hammouri, A. Yahoui and G. Grellet, "A. nonlinear observer for induction motors", in *Electric Machines and Power Systems*, 1999.
- [11] T. Boukhobza, M. Djemai and J-P. Barbot, "Nonlinear sliding observer for systems in output and output derivative injection form", in *Proc. of IFAC World Congress*, Vol. E, pp 299–305, 1996.
- [12] C. Canudas de Wit and J.J.E. Slotine, "Sliding observers in robot manipulators", *Automatica*, Vol. 27, No. 5, pp 859–864, 1991.
- [13] C. Canudas de Wit, N. Fixot and K.J. Astrom, "Trajectory tracking in robot manipulators via nonlinear estimated state feedback", *IEEE Trans on Robotics and Automation*, Vol. 8, No. 1, pp 138–144, 1992.
- [14] S. Drakunov, "Sliding mode observer based on equivalent control method", in *Proc. of the 31th IEEE CDC92*, pp 2368–2369, 1992.
- [15] S. Drakunov and V. Utkin, "Sliding mode observer: Tutorial", in *Proc. of the 34th IEEE CDC95*, 1995.
- [16] M. Djemai, J. Hernandez and J-P. Barbot, "Nonlinear control with flux observer for a singularly perturbed induction motor", *The 32nd IEEE CDC*, San Antonio, USA, pp 3391–3396, 1993.
- [17] M. Djemai, T. Boukhobza, J-P. Barbot, J-L. Thomas and S. Poullain, "Rotor speed and flux nonlinear observer for speed sensorless induction motor", in *Proc. of IEEE-Conf. on Control Application*, 1998.
- [18] A. Damiano, G. Gatto, I. Marongiu, A. Pisano, E. Usai, "Rotor speed estimation in electric drives via digital second order sliding differentiation", *Proceedings of European Control Conference ECC99*, Karlsruhe, Germany, 1999.
- [19] B. Drazenovic, "The invariance Conditions in Variable Structure Systems", *Automatica*, Vol. 5, No. 3, pp. 287–295, 1969.
- [20] C. Edwards and S. K. Spurgeon, "*Sliding Mode Control, Theory and Applications*", Taylor and Francis, London, 1998.
- [21] S.V. Emel'Yanov, "*Variable structure control systems*", Nauka, 1967.
- [22] A.F. Filippov, "*Differential equations with discontinuous right-hand sides*", Ed. Kluwer Academic Publishers, 1988.

- [23] M. Fliess, "Generalized controller canonical forms for linear and nonlinear dynamics", *IEEE-Trans. on AC*, Vol. 35, pp. 994–1000, 1990.
- [24] L. Fridman and A. Levant, "Higher order sliding modes as the natural phenomenon in control theory", in *Robust control via variable structure and Lyapunov techniques*, Ed F. Garafalo and L. Gliemo, Springer-Verlag, Berlin, No. 217, pp 107–133, 1996.
- [25] M. Fliess et J. Rudolph, "Corps de Hardy et observateur asymptotiques locaux pour systèmes différentiellements plats", in *Traitement du signal/ Signal processing*, pp. 1-7, C.R. Acad. Sci. XXX, Paris, 1996.
- [26] J.P. Gauthier, H. Hammouri and I. Kupka, "Observers for nonlinear systems", *The 30th IEEE-CDC*, Brighton, England, pp. 1483–1489, 1991.
- [27] J.P. Gauthier, H. Hammouri and S. Othman, "A simple observer for nonlinear systems: Application to bioreactors", *IEEE Trans. on AC-37*, No. 6, pp. 875–880, 1992.
- [28] J. Hernandez and J-P. Barbot, "Sliding observer-based feedback control for flexible joints manipulator", *Automatica*, Vol. 32, No. 9, pp 1243–1254, 1996.
- [29] A.J. Krener and A. Isidori, "Linearization by output injection and nonlinear observers", *Sys. and Cont. Letters* 3, pp 47–52, 1983.
- [30] A.J. Krener and W. Respondek, "Nonlinear observer with linearizable error dynamics", *SIAM J. Cont. and Opt.*, Vol. 23, pp 197-216, 1985.
- [31] A. Levant, "Sliding order and sliding accuracy in sliding mode control", *Int. J. of Control*, Vol. 58, No. 6, 1247–1253, 1993.
- [32] R. Marino, "High-gain feedback in non-linear control systems", *International Journal of Control*, Vol 42, No 6, pp 1369–1385, 1985.
- [33] W. Perruquetti, T Floquet and P. Borne, "A note on sliding observer and controller for generalized canonical forms", in *Proc. IEEE CDC98*, 1998.
- [34] F. Plestan, "Linearization by generalized input-output injection and synthesis of observers", *Thèse de doctorat, Ecole Centrale de Nantes*, Université de Nantes, 1995.
- [35] J. Rudolph and M. Zeitz, "A block triangular nonlinear observer normal form", *Sys. and Cont. Letters*, 23, pp 1–8, 1994.

- [36] A. Sabanovic, N. Sabanovic and K. Ohnishi, "Sliding modes in power converters and motion control systems", *Int. J. of Control*, Vol. 57, No. 5, pp 1237–1259, 1993.
- [37] H. Sira Ramirez, "On the dynamical sliding mode control of nonlinear systems", *Int. J. of Control*, Vol. 57, No. 5, pp 1039–1061, 1993.
- [38] H. Sira Ramirez and M. Ilic, "Exact Linearization in Switch Mode DC-to-DC Power Converters", *Int. J. of Control*, Vol. 50, No. 2, pp 511–524, 1989.
- [39] H. Sira Ramirez and S.K. Spurgeon, "On the robust design of sliding observers for linear systems", *Sys. and Cont. Letters*, 23, pp 9–14, 1994.
- [40] J.J.E. Slotine, J.K. Hedrick and E.A. Misawa, "Nonlinear state estimation using sliding observers", *The 25th IEEE CDC*, Athens, pp 332–339, 1986.
- [41] J.-J. Slotine and S.S. Sastry, "Tracking control of nonlinear systems using sliding surfaces with application to robot manipulator", *Int. J. of Control*, Vol. 38, No. 2, 1983.
- [42] H.J. Sussman and P.V. Kokotovic, "The peaking phenomenon and the global stabilization of nonlinear systems", *IEEE TAC*, Vol. 36, No. 4, pp 424–440, 1991.
- [43] V. Utkin, "Variable structure systems with sliding modes", *IEEE Trans on AC -22*, No. 2, pp 212–222, 1977.
- [44] Vadim I. Utkin, De-Shiou Chen, Shahram Zerei and John Miller, "Nonlinear Estimator Design of Automotive Alternator utilizing Battery Current and Speed Measurements", *European Journal of Control*, Vol. 6, No. 2, 2000.
- [45] X. Xia and W. Gao, "Nonlinear observer design by observer canonical forms", *Int. J. of Control*, Vol. 47, No. 4, pp 1081–1100, 1988.
- [46] X. Xia and W. Gao, "Nonlinear observer design by observer error linearization", *SIAM J. Cont. and Opt.*, Vol 27, No. 1, pp 199–213, 1989.
- [47] E. Yaz and A. Azemi, "Variable structure with a boundary-layer for correlated noise/disturbance models and disturbance minimisation", *Int. J. of Control*, Vol. 57, No. 5, 1993.

- [48] K.D. Young, V.I. Utkin and U. Ozguner, "A control Engineer's guide to sliding mode control", *IEEE Transactions on Control Systems Technology*, Vol. 7, No. 3, pp 328–342, 1999.
- [49] K.D. Young, U. Ozguner and J-X. Xu, "Variable structure control of flexible manipulators", in *Variable Structure Control for Robotics and Aerospace Applications*, K.D. Young Editor, New York, Elseiver, pp 247–277, 1993.
- [50] A.S. Zinober, "*Varriable Structure and Lyapunov Control*", London, UK, Springer-Verlag, 1993.
- [51] A.S. Zinober, E. Fossas-Colet, J.C. Scarrat and D. Biel, "Two Sliding Mode Approaches to the Control of a Buck-Boost System", *The 5th Int. Workshop on VSS*, Longboat Key, Florida, December 11-13, 1998.