# Vehicle Propulsion Systems Lecture 7

Supervisory Control Algorithms

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November 21, 2012

Outline

#### Repetition

Supervisory Control Algorithms

Heuristic Control Approaches

**Optimal Control Strategies** 

Analytical solutions to Optimal Control Problems

ECMS – Equivalent Consumption Minimization Strategy

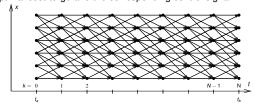
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# Deterministic Dynamic Programming - Basic algorithm

$$J(x_0) = g_N(x_N) + \sum_{k=0}^{N-1} g_k(x_k, u_k)$$
$$x_{k+1} = f_k(x_k, u_k)$$

Algorithm idea:

Start at the end and proceed backward in time to evaluate the optimal cost-to-go and the corresponding control signal.

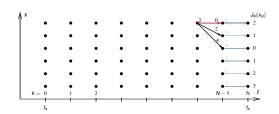


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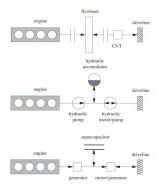
# Deterministic Dynamic Programming – Basic Algorithm

Graphical illustration of the solution procedure



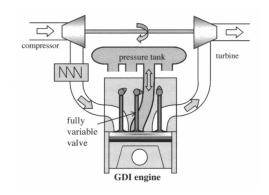
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# **Examples of Short Term Storage Systems**



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# Pneumatic Hybrid Engine System



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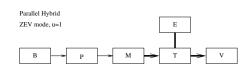
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# Parallel Hybrid - Modes and Power Flows

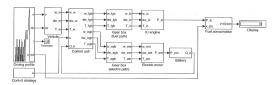
The different modes for a parallel hybrid

 $u \approx P_{batt}/P_{vehicle}$ 

Battery drive mode (ZEV)



# Control algorithms



Determining the power split ratio u

$$u_j(t) = \frac{P_j(t)}{P_{m+1}(t) + P_l(t)}$$
 (4.110)

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- ▶ Clutch engagement disengagement  $B_c \in \{0, 1\}$
- Engine engagement disengagement B<sub>e</sub> ∈ {0, 1}

Strategies for the Parallel Hybrid

Power split u, Clutch  $B_c$ , Engine  $B_e$ 

	Mode	и	$B_e$	$B_c$
1	ICE	0	1	1
2a	ZEV	1	0	0
2b	ZEV	1	0	1
3	Power assist	[0,1]	1	1
4	Recharge	< 0	1	1
5a	Regenerative braking	1	0	0
5a	Regenerative braking	1	0	1

All practical control strategies have engine shut off when the torque at the wheels are negative or zero; standstill, coasting and braking.

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# Classification I - Supervisory Control Algorithms

- Non-causal controllers
  - Detailed knowledge about future driving conditions.
  - Position, speed, altitude, traffic situation.

Regulatory drive cycles, public transportation, long haul operation, GPS based route planning.

- Causal controllers
  - No knowledge about the future...
  - Use information about the current state.
  - Uses:

"The normal controller", on-line, in vehicles without planning

# Classification II - Vehicle Controllers

- ► Heuristic controllers
  - -Causal
  - -State of the art in most prototypes and mass-production
- Optimal controllers
  - -Often non-causal
  - -Solutions exist for simplifications
- Sub-optimal controllers
  - -Often causal

On-going work to include optimal controllers in prototypes

#### Some Comments About the Problem

- ► Difficult problem
- Unsolved problem for causal controllers
- Rich body of engineering reports and research papers on the subject
  - -This can clearly be seen when reading chapter 7!

# Outline

Heuristic Control Approaches

# **Heuristic Control Approaches**

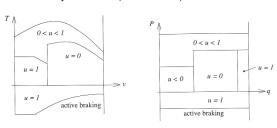
Operation usually depends on a few vehicle operation

- Rule based:  $\textbf{Nested} \; \texttt{if-then-else} \; \textbf{clauses}$ if  $v < v_{low}$  then use electric motor (u=1). else...
- Fuzzy logic based Classification of the operating condition into fuzzy sets. Rules for control output in each mode. Defuzzyfication gives the control output.

# **Heuristic Control Approaches**

torque demand.

Parallel hybrid vehicle (electric assist)



 Determine control output as function of some selected state variables: vehicle speed, engine speed, state of charge, power demand, motor speed, temperature, vehicle acceleration,

# Heuristic Control Approaches - Concluding Remarks

- ► Easy to conceive
- ► Relatively easy to implement
- ► Result depends on the thresholds
- Proper tuning can give good fuel consumption reduction and charge sustainability
- Performance varies with cycle and driving condition –Not robust
- Time consuming to develop an tune for advanced hybrid configurations

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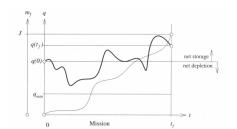
#### **Optimal Control Strategies**

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# Consider a driving mission

Variables. Control signal − u(t), System state − x(t), State of charge q(t) (is a state).



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# Formulating the Optimal Control Problem

-What is the optimal behaviour? Defines Performance index J.

▶ Minimize the fuel consumption

$$J = \int_0^{t_f} \dot{m}_f(t, u(t)) dt$$

▶ Balance between fuel consumption and emissions

$$J = \int_0^{t_f} \left[ \dot{m}_f(t, u(t)) + \alpha_{CO} \dot{m}_{CO}(x(t), u(t)) + \alpha_{NO} \dot{m}_{NO}(x(t), u(t)) + \alpha_{HC} \dot{m}_{HC}(x(t), u(t)) \right] dt$$

Include driveability criterion

$$J = \int_0^{t_f} \dot{m}_f(t, u(t)) + \beta \left(\frac{d}{dt}a(t)\right)^2 dt$$

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#### First Solution to the Problem

► Minimize the fuel consumption

$$J = \int_0^{t_f} \dot{m}_f(t, u(t)) dt$$

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#### Including constraints

Hard or soft constraints

$$min J(u) = \int_{t_a}^{t_b} L(t, u(t)) dt$$
s.t.  $q(0) = q(t_f)$ 

$$\min \ J(u) = \phi(q(t_f)) + \int_{t_a}^{t_b} L(t,u(t)) dt$$

▶ How to select  $\phi(q(t_f))$ ?

$$\phi(q(t_f)) = \alpha (q(t_f) - q(0))^2$$

penalizes high deviations more than small, independent of sign

$$\phi(q(t_f)) = w(q(0) - q(t_f))$$

penalizes battery usage, favoring energy storage for future use

One more feature from the last one

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# Including constraints

► Including battery penalty according to

$$\phi(q(t_f)) = w(q(0) - q(t_f)) = w \int_0^{t_f} \dot{q}(t)dt$$

enables us to rewrite

$$\min \ J(u) = \int_{t_a}^{t_b} L(t, u(t)) + w \, \dot{q}(t) dt$$

#### Constraints That are Also Included

- State equation  $\dot{x} = f(x)$  is also included From Lecture 5
- Consider hybrid with only one state, SoC

$$\begin{aligned} \min J(u) &= \phi(q(t_b), t_b) + \int_{t_a}^{t_b} L(t, u(t)) dt \\ s.t. &\frac{d}{dt}q = f(t, q(t), u(t)) \\ &u(t) \in U(t) \\ &q(t) \in Q(t) \end{aligned}$$

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▶ Core of the problem

$$\begin{aligned} & \text{min } J(u) = \phi(q(t_b), t_b) + \int_{t_a}^{t_b} L(t, u(t)) dt \\ & s.t. \ \dot{q}(t) = f(t, q(t), u(t)) \end{aligned}$$

► Hamiltonian from optimal control theory

$$H(t, q(t), u(t), \mu(T)) = L(t, u(t)) + \mu(t) f(t, q(t), u(t))$$

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# Analytical Solutions to Optimal Control Problems

Hamiltonian

$$H(t, q(t), u(t), \mu(T)) = L(t, u(t)) + \mu(t) f(t, q(t), u(t))$$

► Solution (theory from chapter 9)

$$u(t) = \underset{u}{\operatorname{arg\,min}} H(t, q(t), u(t), \mu(T))$$

with

$$\dot{\mu}(t) = -\frac{\partial}{\partial q} f(t, q(t), u(t))$$
$$\dot{q}(t) = f(t, q(t), u(t))$$

▶ If  $\frac{\partial}{\partial q}f(t,q(t),u(t))=0$  the problem becomes simpler  $\mu$  becomes a constant  $\mu_0$ , search for it when solving

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# Analytical Solutions to Optimal Control Problems

 $ightharpoonup \mu_0$  depends on the (soft) constraint

$$\mu_0 = rac{\partial}{q(t_f)}\phi(q(t_f)) = / ext{special case}/ = -w$$

▶ Different efficiencies

$$\mu_0 = \frac{\partial}{\partial \textit{q}(\textit{t}_\textit{f})} \phi(\textit{q}(\textit{t}_\textit{f})) = \begin{cases} -\textit{w}_\textit{dis}, & \textit{q}(\textit{t}_\textit{f}) > \textit{q}(0) \\ -\textit{w}_\textit{chg}, & \textit{q}(\textit{t}_\textit{f}) < \textit{q}(0) \end{cases}$$

 Introduce equivalence factor (scaling) by studying battery and fuel power

$$s(t) = -\mu(t) \frac{H_{LHV}}{V_b Q_{max}}$$

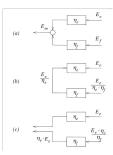
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# Determining Equivalence Factors I

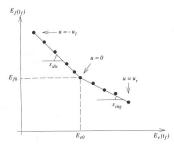
Constant engine and battery efficiencies

$$egin{aligned} oldsymbol{s}_{ extit{dis}} &= rac{1}{\eta_e\,\eta_i} \ oldsymbol{s}_{ extit{chg}} &= rac{\eta_e}{\eta_i} \end{aligned}$$



Determining Equivalence Factors II

 Collecting battery and fuel energy data from test runs with constant u gives a graph

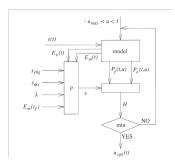


► Slopes determine  $s_{dis}$  and  $s_{chg}$ .

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# **ECMS On-line Implementation**

Flowchart



There is also a T-ECMS (telemetry-ECMS)